HELL 2D.
HUNTSBURG TP.

115

LEVEL BOOK

373

KEUFFEL & ESSER CO.

DRAWING MATERIALS
AND
SURVEYING INSTRUMENTS.
NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS SECTIONING.
ROADWAY 0 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

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PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250-X

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julion A. Hall, M. Am. Soc. C. E.

~~Hell Road~~ (Pioneer Rd) - T.H. 116

Benchmarks - pg - 1-3

X-Sections - pg - 4-23

Slope Stakes - pg - 24-40

Drainage - Sec. D - pg - 40-46

(115)

BENCH MARKS

B. M. #1 X on N. E. Corner N. H'd Wall
Side Rd. Culvert Sta 0+15
Elev. 1135.475

B. M. # 2 Spike in W. Root 16" Hickory
42' Lt. Sta 11+73
Elev. 1118.685

B. M. #3 Spike in N. Root 18" Hickory
115' Lt. Sta 19+36
Elev. 1118.39

B. M. # 4 Spike in N. Root 26" Maple
42' Lt. Sta 26+70
Elev. 1117.175

B. M. #5 Bent Spike in N. Root
12" Maple 23' Lt. Sta 37+91
Elev. 1100.39

B. M. #6 Spike in N. Side 10" Maple
20' Lt. Sta 42+49
Elev. 1099.36

B. M. #7 Spike in S.W. Side 40" Elm
42' Lt. Sta 49+57
1089.01

B. M. #8 Spike in So. Side 16" Apple
30' Lt. Sta 52+30
Elev. 1101.555

B. M. #9 Bent Spike in N.W. Root
26" Maple 20' Rt. Sta 60+82
Elev. 1081.135

B. M. #10 Bent Spike in N. Root
14" Maple 25' Rt. Sta 66+78
Elev. 1109.24

B. M. #11 Spike in N. Root 12" Maple
21' Rt. Sta 75+52
Elev. 1112.11

B. M. #12 Spike in N.W. Root
24" Stump 18' Rt.
Sta 81+42
Elev. 1109.60

B. M. #13 Bent Spike in N.W. Root
18" Elm 20' Rt.
Sta 87+67
Elev. 1107.935

B. M. # 14 Spike in N. Side
24" Elm 18' Rt. Sta 99+05
Elev. 1105.99

B. M. # 15 Spike in S. W. Root
10" Poplar 50' Lt.
Sta 105+17
Elev. 1100.51

B. M. # 16 Spike in N. W. Root
16" Maple (S) 31' Rt.
Sta 113+62
Elev. 1095.635

B. M. # 17 Spike in W. Root
18" Maple 50' Rt.
Sta 121+40
Elev. 1094.82

B. M. # 18 Spike in N. Side 8" Elm
50' Rt. Sta 127+75
Elev. 1088.88

B. M. # 19 Spike in N. Root
24" Maple 17' Rt.
Sta 132+88
Elev. 1084.47

HELL RD. (HU TSBURG TP.) S. Gold Jr. S. Merritt H. Barton 7-14-30

Sta	+	H.I.	-	Elev.	Rem's	South	℄	North
B.M.	5.67	1141.145		1135.475	X. N.E. Corner N. Hdwall Side Rd. Culvert Sta 0+15 El. 1135.475			
0+0		℄ Pavement				5.45/50' 5.34/30	4.74	3.71/30' 2.86/50'
+07		E. Edge Pave				5.46/50 5.37/30	4.80	4.0/30' 2.99/50'
+15	℄ Culvert					9.0/40 8.5/F.L. 13 6.7/13 6.7/12	5.9	5.9/26 5.7/26 5.7/27 8.0/F.L. (27') 6.9/50
+40						9.2/30 9.4/24 9.3/16 9.2/12 9.7/6	8.9	8.5/4 8.1/14 8.6/20 8.1/25 6.8/30
1+0						10.2/30 9.7/22 10.0/15 9.7/8 10.2/7 9.9/4	9.3	9.2/7 9.8/15 9.3/17 9.6/22 9.8/23 9.8/30
2+0						11.2/30 11.0/15 10.3/14 10.0/10 10.3/7 10.7/5	9.8	9.7/6 9.9/12 10.6/15 10.1/17 10.1/30
T.P.	7.88	1138.905	10.12	1131.025				
3+0						9.4/30 8.8/23 8.5/19 8.2/9 8.7/7	7.9	7.7/3 8.0/8 8.4/11 8.9/13 8.4/14 8.2/20 8.1/25 7.4/27 7.1/30
+61	℄ Culvert					10.8/100 10.0/60 9.4/30 9.2/21 8.9/11 8.9/F.L. (7) 8.5/5 11.3/150 12.9/225 → 150' at Rt. ∠'s to ℄; 215 ℄ Creek	7.9	7.7/4 8.3/9 8.7/F.L (9) 9.1/11 8.4/14 8.2/20 7.2/30
4+0						9.4/30 9.5/23 8.5/18 9.3/15 8.8/14 8.7/10	8.1	7.9/3 8.2/9 8.9/11 8.5/14 8.0/19 7.7/24 6.9/30

Sta	+	H.I. 1138.905	−	Elev	Rem's
5+0					
T.P.	2.595 (4.0)	1138.86	2.64	1136.265	
+24					
6+0					
7+0					
T.P	2.565	1128.855	12.57	1126.29	
8+0					
9+0					
10+0					
T.P.	3.70	1122.055	10.50	1118.355	
11+0					
B.M			3.37	1118.685	
+44	℄ Culvert (No Outlet Ditch thru the pasture) Pres. Road Ditch (South Side) Carries the Water Clear to the Next Culvert's Outlet (2' Ditch Slon Both Sides of Rd. Pres. Culvert to be Replaced With a New Hillside Culvert				

South ℄ North

3.8/30 3.4/26 2.9/22 3.7/19 5.1/14 6.5/12 5.8/9 5.1 5.5/8 6.0/10 4.7/12 3.0/17 1.8/21 1.3/25 0.8/30

2.9/30 2.7/25 2.2/23 3.3/17 5.2/13 5.8/12 5.3/10 4.4 4.8/7 5.4/10 3.8/13 3.5/16 2.4/18 1.5/27 1.5/30

4.5/30 4.2/24 7.2/14 8.0/12 6.5/7 6.4 6.7/7 7.7/10 6.4/12 5.4/18 4.8/25 4.8/30

7.4/30 7.3/25 7.9/20 10.9/11 12.1/10 10.8/7 10.5 10.7/5 12.0/8 10.1/11 9.9/14 10.2/17 10.1/30

4.9/30 5.3/22 5.5/14 6.5/13 5.9/9 5.4/4 5.8 6.2/3 5.1/5 7.3/9 7.5/12 5.9/16 5.1/25 5.2/30

8.0/30 7.6/21 8.7/17 8.4/14 9.1/11 8.4/7 8.6 8.8/3 9.2/6 7.8/7 7.2/9 9.0/13 8.9/16 8.1/19 8.2/30

10.3/30 11.0/21 11.7/20 11.5/14 10.6/11 11.3/9 10.6/3 10.7 10.6/8 8.7/10 9.3/13 9.9/16 9.7/19 9.6/30

4.0/30 4.3/21 5.7/17 5.6/15 3.3/10 4.6/9 4.5 4.5/9 4.7/11 3.1/14 4.3/17 4.4/21 3.2/22 3.4/30

4.2/35 4.3/22 5.8/15 3.9/9 6.0/F.L → 4.5/3 4.4 4.6/13 5.1/F.L (13) 4.9/16 5.1/32 4.9/30

5.7/42 * 5.9/42

Sta	+	H.I.	-	Elev.	Rem's	South — ℄ — North
B.M.	3.39	1122.075		1118.685	Spike in W Root 16" Hickory 42' Rt of Rd. Sta 11+73 El. 1118.685	
12+0						5.2/30 5.3/23 6.2/20 6.4/16 6.7/13 3.8/7 5.3/5 4.6 4.9/9 5.2/11 3.9/14 5.4/16 5.9/19 4.4/21 3.8/30
13+0						5.1/30 5.1/18 6.7/16 7.2/14 4.7/11 4.1/8 5.2/6 4.8 5.4/10 4.8/11 6.5/14 7.0/17 5.0/20 4.3/30
14+0						5.5/30 5.5/22 7.5/20 7.4/18 3.9/11 4.1/8 4.2 4.6/6 4.1/8 5.3/10 7.4/13 7.5/15 4.9/19 5.0/30
+68.5	℄ Culvert (Pres. Culvert is Large Enough and is in Good Condition.					7.8/85 8.3/28 7.8/F.L. → 1.6/13.6 1.6/12.1 2.7/11 2.7/10 3.5/9 3.4 3.3/3 2.7/5 1.5/5 1.5/6.5 ← F.L. 7.9 7.6/12 7.5/F.L. 5.6/20 5.1/50
	8.3/160 9.4/250					↳ 4" Tile 14' N. of ℄
outlet	Channel to be Cleaned for 250') A 4" Tile Across the Northfield Drains into the Culvert.					
T.P	1.06	1121.675	1.46	1120.615		
15+0						5.1/30 5.3/21 5.6/17 4.3/9 4.2 5.9/10 6.1/11 4.9/13 5.1/18 5.1/30
16+0						6.1/30 5.0/19 5.2/15 5.5/14 5.0 5.8/7 4.9/10 4.9/30
17+0						1.7/30 0.6/24 3.7/17 4.9/16 3.6/11 3.4 3.8/3 4.9/8 3.6/9 4.0/12 1.8/17 1.9/30
T.P.	5.18	1123.865	2.99	1118.685		
18+0						4.1/30 3.8/25 4.9/21 5.4/16 6.0/14 5.2 5.3/3 6.2/7 5.4/8 4.6/13 4.0/18 4.2/30

Sta	+	H. I.	−	Elev.	Rem's
19+0		1123.865			
B.M.			5.475	1118.39	Spike in N. Root 18" Hickory 11.5' S. of ℄ Sta 19+36
20+0					
+30					
21+0					
T.P.	4.42	1121.025	7.26	1116.605	
22+0					
23+0					
T.P.	5.54	1120.955	5.61	1115.415	
24+0					
25+0					
26+0					
T.P.	1.655	1117.87	4.74	1116.215	
27+0					

South ℄ North

6.1/30	5.5/14	6.3/12	5.7/11	5.2/8	5.0	5.2/3	6.3/8	5.5/9	5.5/16	5.5/30
2.8/30	3.4/16	5.5/11	4.6/6		4.3	4.7/4	5.3/8	5.9/10	4.6/13	3.7/18	4.2/30
2.4/30	3.0/20	3.7/15	5.6/11	4.5/7	4.0	4.6/5	5.8/10	4.5/14	3.9/22	4.6/30	
3.9/30	4.3/14	5.5/11	5.7/9	6.7/8	5.8/5	5.5	5.8/5	7.0/9	5.9/11	4.9/12	4.8/22	5.6/30
4.0/30	3.5/19	4.7/12	5.9/10	4.5/6	4.3	4.7/6	5.8/10	5.0/12	4.4/15	3.9/17	3.7/21	4.4/30
5.9/30	5.8/12	6.8/11		5.8/8	5.4/5	5.4	5.6/4	6.2/8	6.7/9	6.0/11	6.2/30	
5.9/30	5.7/14	6.7/11	5.5/9		5.2	5.9/6	6.2/7	5.7/9	5.8/30		
5.0/30	4.7/17	5.3/12	6.0/11	4.8/6	4.5/3	4.7	5.0/3	5.7/6	5.1/9	6.0/30		
2.8/30	3.7/14	5.6/10	4.9/8		4.3	4.6/4	5.7/8	4.9/9	5.3/30		
3.1/30	3.2/14	4.8/10	4.1/5		4.1	4.5/5	5.3/6	4.0/8	3.1/18	2.9/30		

Sta	+	H.I. 1117.87	−	Elev.	Rem's
B.M.			0.695	1117.175	Spike in N. Root 26" Maple 42' Lt. Sta 26+70
28+0					
29+0					
T.P.	2.93	1111.36	9.44	1108.43	
30+0					
31+0					
32+0					
+42	℄	Drive	North		
T.P.	2.47	1105.96	7.87	1103.49	
33+0					
34+0					
35+0					

South ℄ North

6.7/30 5.9/27 6.2/20 7.0/17 8.1/11 7.1/6 6.9 7.1/3 7.9/7 7.0/9 5.7/30

9.5/30 8.4/27 8.0/24 8.9/21 8.6/12 9.4/11 8.7/5 8.5 8.8/4 9.3/7 9.0/11 9.1/30

3.5/30 2.7/25 2.3/22 3.0/19 4.0/11 4.8/10 4.2/8 3.5/5 3.2 3.7/5 5.1/8 4.5/10 3.4/15 4.2/30

4.8/25 3.7/22 4.5/13 4.7/30 5.2/11 7.0/9 6.5/7 5.9/3 5.7 6.1/6 6.8/9 6.2/11 5.0/14 4.9/30

7.9/30 8.1/25 7.4/17 7.6/10 8.7/8 7.8/5 7.5 7.5/6 7.9/8 8.6/10 7.9/12 7.2/17 5.9/30 4.1/H

8.0 8.0/8 7.4/30

4.6/30 4.7/25 3.4/20 3.7/16 3.8/10 4.7/8 3.9/5 3.4 3.6/8 4.1/12 4.6/13 3.9/15 3.3/19 3.1/26 2.9/30

4.9/30 4.7/25 4.3/18 4.7/16 4.9/10 5.5/7 4.8/5 4.7 4.3/5 5.1/11 5.7/13 4.8/15 3.9/30

5.6/30 5.3/20 5.7/10 6.1/8 5.4/7 5.0 5.5/10 6.5/13 5.5/16 5.7/30

Sta	+	H.I.	−	Elev.	Remarks
35+50		1105.96		℄ Drive South	
36+0					
37+0					
T.P. & B.M.	3.755	1104.145	5.57	1100.39	Bent Spike in N. Root 12" Maple 23' Lt. Sta 37+91
38+0					
39+0					
40+0					
41+0					
+11	℄	Drive	North		
42+0					
T.P. & B.M.	3.135	1102.495	4.785	1099.36	Spike in N. Side 10" Maple 20' Lt. Sta 42+69
43+0					

South ℄ North

5.3/30 5.8/15 5.8

6.1/30 6.1/14 6.6/10 7.1/7 6.5/5 6.7 6.5/10 6.9/12 6.4/14 5.8/30

6.7/30 6.8/19 6.7/10 7.5/9 6.9/6 6.5 6.5/7 6.9/10 7.2/12 6.8/14 6.5/30

5.2/30 5.4/20 5.2/11 6.2/9 5.3/7 4.6 5.1/9 5.9/12 5.0/15 4.8/24 4.6/30

5.1/30 5.2/21 5.5/11 6.3/10 5.5/7 4.8 5.5/13 6.2/15 5.2/18 5.2/23 5.5/30

5.0/30 5.4/13 6.4/11 5.7/9 4.9 5.4/10 6.5/12 5.7/14 5.8/24 5.9/30

5.0/30 5.1/22 5.4/14 6.4/12 5.7/10 5.0 5.6/10 6.3/12 5.7/13 5.2/15 5.3/30 5.7/H.

5.0 5.6/12 5.4/30

5.1/30 5.8/17 6.1/14 7.2/11 6.3/10 5.4/5 5.3 5.7/8 7.0/12 5.6/14 4.9/24 4.9/30

4.5/30 4.8/17 5.3/11 6.8/9 6.8/7 5.1/5 4.8 4.9/5 6.3/10 4.7/12 4.0/30

HELL RD. HUNTSBURG

Sta	+	H.I.	-	Elev.	Rem's
44+0		1102.495			
45+0					
+25					
+82	℄	Drive	North		
46+0					
T.P.	2.19	1096.535	8.15	1094.345	
47+0					
+95	℄	Culvert (Outlet Channel Runs parallel to Rd.)			
48+0		(on the Culvert)			
T.P.	7.53	1096.415	7.65	1088.885	
+46	℄	Culvert			
49+0					

TWP JULY 16 '30 — S. Gold Jr. S. Merritt H. Barton — 10

South ℄ North

5.5/30	5.8/14	6.1/10	8.1/9	7.7/7	6.0/5	5.6	6.0/8	7.4/10	7.3/11	5.9/12	5.1/30
5.6/30	6.0/18	6.6/13	9.9/8	9.8/6	8.0/3	7.7	7.9/7	8.6/8	8.3/10	7.0/12	5.8/30
6.3/30	6.6/15	7.9/13	10.2/10	10.0/8	7.9/5	7.7	7.8/6	8.8/8	8.7/10	7.1/13	6.7/21	6.2/30
						9.2	9.7/10	8.4/21	8.1/30	4.7/H	
8.2/30	8.0/27	8.0/15	9.1/12	11.5/10	11.4/8	10.2/5	9.7	9.9/8	10.4/10	8.3/14	8.1/17	7.6/30
6.8/30	6.1/14	5.6/12	6.1/9	6.5/7	6.1/6	5.6	5.9/9	7.2/12	6.4/13	6.7/30		
10.1/50	10.3/30	9.8/F.L.	3.7/10	3.7/8.5	5.2/8.5	5.8	5.2/8.5	3.7/8.5	3.7/10	9.9/F.L.	8.8/22	8.9/28
9.0/200	8.2/300											
8.1/30	8.7/2	9.9/10	3.6/10	3.6/8.5	5.6/8.5	5.5/7	6.1/5	6.0	5.9/5	5.3/8	3.7/8.5	3.7/10	10.1/10	9.4/19	8.8/27
															7.8/30
7.8/30	7.9/12	9.4/10	9.5/F.L.	8.5/5	8.3/4	8.2	8.1/8	8.6/11	9.4/F.L.	9.6/16	10.5/21	10.4/23	9.1/25
										7.6/30	8.3/50		
7.6/30	7.5/17	7.9/10	9.0/7	7.9/3	7.9	8.4/12	7.5/14	8.9/16	9.6/20	11.8/22	11.5/27		
								9.7/29	8.7/34	8.3/50			

Sta	+	H.I.	-	Elev.	Rem's
49+50		1096.415			
B.M.			7.405	1089.01	Spike in S.W side 40" Elm 42' Lt. Sta 49+57
50+0					
51+0	℄ Creek	76' N. of ℄			
T.P.	6.94	1102.17	1.185	1095.23	
52+0					
+50					
+92	℄	Drive South			
53+0					
B.M.			0.615	1101.555	Spike in S Side 16" Apple 30' Lt. Sta 52+30
54+0					
+03	℄	Culvert			
55+0					

South ℄ North

3.8/30 4.5/19 5.6/12 8.2/8 8.4/6 7.5/3 7.5 7.5/8 8.4/12 10.0/14 11.4/19 11.0/24 10.1/27 9.2/31
8.4/32 8.9/35 8.8/41 8.9/47 8.1/50

4.0/30 4.2/22 5.1/15 7.6/8 6.9/5 6.5 6.8/9 7.4/13 6.9/15 7.3/18 10.5/21 11.5/25 11.6/29
10.9/30 9.7/39 8.6/41 8.6/45

2.2/30 2.1/24 2.8/15 5.1/10 4.2/6 3.7 4.1/8 5.2/11 4.4/13 3.5/17 1.9/19 2.3/23 5.1/30
6.2/35 9.3/41 10.6/72 11.8/72 11.7/80
10.7/86 9.8/90

4.5/30 4.9/21 5.8/16 7.2/14 6.0/10 5.8 6.1/5 7.0/8 6.1/9 5.5/12 3.8/19 3.5/30

1.1/14 2.9/30 3.2/19 4.9/13 4.2/7 3.9 4.4/5 5.2/8 4.2/10 2.6/16 2.6/30

3.9/45 4.1/30 3.7/16 5.5/8 5.0

3.7/30 4.7/24 5.7/11 5.4 5.7/6 6.2/9 5.6/10 5.5/14 4.5/16 5.0/18 5.0/30

6.1/30 6.6/22 6.7/11 7.1/9 6.1/7 5.7 6.2/6 7.2/10 6.3/11 6.9/18 7.1/30

6.8/50' 6.1/F.L. 6.9/30 6.6/12 7.1/10 7.1/F.L. 6.2/8 5.7 6.2/6 6.5/8 7.3/F.L. 7.7/24 9.2/45 10.4/70
4" Tile 23' South

4.1/30 4.7/13 5.8/10 5.3/8 4.9 5.2/5 5.7/8 4.9/9 4.2/10 3.9/30

Sta	+	H.I.	−	Elev	Remarks
55+40		1102.17			
T.P.	2.60	1100.34	4.43	1097.74	
56+0					
57+0					
58+0					
59+0					
T.P.	1.96	1090.74	11.56	1088.78	
60+0					
60+75					
B.M. & T.P.	8.73	1089.365	9.605	1081.135	Bent Spike in N.W. Root 22" Maple 30° Rt. Sta 60+82
60+90					
61+0					
+17.5	West	About 4			

South ℄ North

3.3/30	3.9/14	4.8/11	4.1/8	3.6	4.1/5	5.0/6	3.8/11	4.1/30	
1.9/30	2.9/17	2.8/12	3.5/11	2.8/8	2.4	3.0/6	3.6/8	2.6/10	2.8/30
3.0/30	3.2/21	2.8/12	5.3/9	4.4/6	4.2	4.5/7	5.4/9	3.8/12	4.1/30
4.9/30	5.6/20	7.2/10	9.8/6	8.8/4	8.5	8.9/7	9.3/8	6.6/13	6.4/30
12.3/30	12.7/16	12.0/12	12.8/9	12.4/5	12.2	12.2/7	12.9/9	12.2/12	12.7/30
4.9/30	5.5/21	5.3/15	5.1/8	4.4/5	4.3	4.8/7	5.4/9	5.1/10	5.5/12	5.5/14	5.1/16	4.8/30
9.4/30	8.2/26	7.8/17	6.6/12	6.2/8	5.1/4	5.0	5.1/8	5.5/11	6.3/16	6.5/24	6.1/30	
13.4/30	12.6/22	10.3/15	9.2/8	5.6/7	3.6/4	3.6	3.6/9	4.6/13	5.4/20	6.0/30		
13.6/30	14.0/22	13.0/8	4.9/7	3.5/4	3.6	3.5/8	7.3/14	8.9/21	8.1/27	7.6/30		
16.0/Gr.L.	4.0/5.8 Top About 4	3.0/4.8	3.1	3.0/7.2	3.9 Top About 8.2	14.6/Gr.L.						

5+2	+	H.I. 1089.365	-	Elev Rem's
61+36	℄ Bridge			
61+53.5				
T.R.	11.725	1100.465	0.625	1088.74
62+0	Top of River Bank			
63+0				
+42.2	℄ Rd. South			
T.R.	10.70	1109.16	2.005	1098.46
+84				
+95	℄ Drive North			
64+0				
65+0				
T.P.	8.06	1113.06	4.16	1105.00
66+0				

South ℄ North

16.1 Bot. Crk | 14.7 W.El. | 2.9/5.1 | 2.9 | 2.9/8.0 | 15.0 W.El. | 16.4 Bot Creek

13.2 Grl. | 3.7 T.A. 6+ 2.6 | 2.8/5.5 | 2.7 | 2.9/6.5 | 3.8 Top A.I.H. 7.5 | 14.3 Grl.

14.2/24, 11.6/30 | 15.4/21 | 15.4/19 | 13.3/18 | 12.4/9 | 12.8/8 | 12.8 | 12.8/6 | 13.3/8 | 12.3/10 | 9.3/20 | 8.7/30

7.1/24 | 8.4/22 | 8.4/20, 6.0/25 | 6.7/17 | 6.6/14 | 7.9/12 | 8.3 | 8.5/4 | 9.0/6 | 8.2/8 | 5.9/12 | 2.8/21 | 2.0/30

2.6/50, 0.7/100 | 3.2/30 | 6.0 E.F.L. | 6.4 W.F.L. | 3.4/22 | 5.1/8 | 5.5 | 5.3/4 | 6.1/6 | 4.0/9 | 3.6/12 | 0.5/19 | +0.7/30

10.5/30 | 10.1/21 | 10.6/19 | 11.8/15 | 10.8/13 | 11.1/8 | 11.4 | 11.0/6 | 12.2/8 | 10.6/10 | 9.7/14 | 7.3/20 | 6.6/30

10.8 | 10.6/5 | 10.1/8 | 8.4/30 | 8.1/33

9.4/30 | 8.6/25 | 8.8/22 | 10.3/18 | 11.3/16 | 10.1/11 | 10.4 | 10.1/4 | 10.7/8 | 9.6/11 | 8.1/22 | 7.9/25 | 7.4/30

3.1/30 | 3.0/15 | 4.6/13 | 7.3/9 | 5.4/6 | 6.2 | 5.4/2 | 6.7/10 | 5.0/12 | 2.7/18 | 2.5/21 | 2.4/30

5.2/30 | 5.4/22 | 5.8/14 | 7.6/11 | 6.1/8 | 5.9 | 6.1/8 | 7.5/12 | 6.1/13 | 5.9/21 | 5.9/26 | 7.0/28 | 6.7/30

Sta	+	H.I. 1113.06	−	Elev.	Rem's
B.M.			3.82	1109.24	Bend Spike in N. Root 14" Maple 25' Rt. Sta 66+78
67+0					
68+0					
69+0					
T.P.	10.80	1119.86	4.00	1109.06	
70+0	Also ℄ Drive North.				
71+0					
71+72	℄ Drive South				
72+0					
+28				16.3	
73+0					
T.P.	3.14	1116.32	6.68	1113.18	

South ℄ North

4.2/30 4.6/25 4.9/18 5.2/11 6.0/9 4.9/6 4.6 4.8/8 5.4/10 6.5/12 5.4/15 5.4/23 5.7/27 6.3/28 6.0/30

2.9/30 3.2/22 4.4/10 5.0/8 4.4/5 4.0 4.2/10 5.4/12 4.2/14 4.3/22 4.4/28 5.3/30

2.0/30 2.5/21 3.2/9 4.2/7 3.4/4 3.1 3.2/10 4.4/12 2.9/14 3.1/24 3.1/27 3.8/28 3.7/30

7.9/30 8.2/21 8.8/9 9.8/6 9.2/4 8.9 9.1/10 9.4/11 8.8/13 8.8/30 8.4/4

5.3/30 4.9/24 5.5/18 6.4/9 7.9/7 7.2/4 6.9 7.1/10 8.2/12 6.7/15 6.1/17 6.5/29 6.7/30

+0.7/4 4.6/30 4.8/12 5.6/8 5.0

3.3/30 3.4/21 4.0/12 4.8/6 4.2 4.0/4 4.3/7 5.4/13 4.8/15 4.1/25 4.8/30

2.8/26 2.4/23 3.3/10 3.4/27 3.2/30 4.2/8 4.5/6 4.1/5 3.6 3.4/4 3.8/10 4.9/14 4.5/16 4.6/30

4.8/30 4.8/27 4.7/13 5.5/11 5.7/7 7.1/6 6.2/3 5.9 5.7/4 6.0/10 6.7/13 6.2/17 6.2/30

Hill Rd. (Huntsburg TP.)

Sta	+	H.I.	−	Elev	Remks
74+0		1116.32			
75+0					
B.M.			4.21	1112.11	Spike in N. Root 12" Maple 21' Rt Sta 75+52
76+0					
B.M.	2.555	1114.665		1112.11	
77+0					
78+0				09.2	
79+0					
T.P.	4.10	1113.17	5.595	1109.07	
80+0					
81+0					
B.M.			3.57	1109.60	Spike in N.W. Root 24" Stump 18' Rt. Sta 81+42
82+0					
83+0				08.0	

July 17, 30

S. Gold
S. Merritt
H. Bardon

15

South ℄ North

4.5 27	3.7 24	4.1 17	4.5 13	4.8 7	5.5 6	4.6 3	4.5	4.6 10	5.3 13	4.8 16	4.5 30
4.9 30										
4.4 30	4.7 24	5.1 14	5.6 11	6.4 6	5.9 4	5.6	5.6 10	6.2 14	5.8 19	5.7 30	
6.1 24	5.9 18	6.6 11	6.3 8	7.2 6	6.4 3	6.2	6.4 8	7.0 12	6.5 18	6.2 30	
6.3 30										
5.8 30	6.3 25	5.4 24	5.7 10	5.4 9	6.2 8	5.4 4	5.0	5.3 9	6.3 11	5.8 14	5.3 30
6.0 30	6.5 24	5.8 23	6.1 9	6.6 7	5.8 4	5.5	5.6 9	6.7 13	6.1 14	5.2 30	
6.4 30	7.0 24	6.3 22	6.5 17	6.4 8	6.9 7	6.1 4	6.3	6.0 9	7.0 13	6.4 14	6.1 30
5.3 30	5.5 23	4.9 21	5.0 18	5.1 6	5.8 4	5.1 2	5.1	4.7 7	5.2 12	6.0 15	5.5 16	5.2 30
5.2 30	5.2 20	5.2 5	6.1 4	5.2	4.6 5	5.1 12	6.1 16	5.1 18	5.0 30		
5.3 30	5.0 19	5.1 5	6.2 4	5.0	4.7 5	5.0 11	6.2 16	5.3 17	5.2 20	5.3 25	4.7 30
5.5 30	5.2 19	5.5 5	6.5 4	5.2	4.9 6	5.1 12	6.7 15	5.4 17	5.5 20	5.8 24	5.3 30	

St	+	H.I.	-	Elev	Rem's
		1113.17			
84+0					
T.P.	5.30	1112.82	5.65	1107.52	
85+0			5.8	1107.0	
+13	℄	Culvert			
+40	℄	Drive	North		
86+0					
87+0					
+10	℄	Drive	South		
88+0					
88+94	℄	Culvert			
89+0					

South ℄ North

5.8/30 5.8/27 5.2/20 5.5/5 6.6/3 5.6 5.1/6 5.6/13 6.5/16 5.5/20 5.7/24 5.2/30

5.6/30 5.8/27 5.4/7 6.3/3 5.8 5.1/7 5.4/15 6.3/18 5.7/21 5.3/30

8.2/300 8.0/250' 8.1/200 8.0/150 7.3/65 6.6/15 6.5/FL (11) 5.5 6.0/8 5.1/14 6.7/FL (15) 5.4/20 5.2/30
8.0/350'

5.7 4.8/8 4.9/17 4.5/30 (1.6/H)

5.7/30 5.9/27 6.5/25 5.3/22 5.3/7 5.8 5.0/3 4.7/9 4.9/14 6.1/17 4.7/19 4.6/21
4.3/30

3.6/30 3.7/26 3.3/23 3.1/16 3.9/6 4.5 4.4/12 5.7/17 4.9/19 4.2/20 4.0/25 4.1/30

(1.6/H) 3.5/30 3.6/22 4.7

5.2/30 5.0/23 6.3/17 5.9/7 6.3/5 5.5 5.4/4 5.7/9 6.9/13 5.9/14 5.6/16 6.2/30

5.8/100' 6.1/55 6.0/9 6.7/8 6.3/FL 5.5/7 5.3 5.5/10 6.3/FL 6.8/11 6.3/15 6.7/16 6.2/22 6.2/30 6.4/50
6.4/100'

5.9/30 6.0/17 6.1/9 6.5/7 5.7/5 5.4 5.5/9 6.8/12 5.9/13 5.9/15 6.7/30

Sta	+	H.I.	−	Elev.	Rem's
90+0		1112.82			
B.M.	4.525	1112.46	4.885	1107.935	Bent Spike in N.W. Root 18" Elm 20' Rt Sta 89+67
91+0					
92+0					
93+0					
T.P.	6.43	1114.02	4.87	1107.59	
94+0					
95+0					
96+0					
+70					
97+0					
98+0					

South ℄ North

5.6/30 5.5/20 5.7/13 6.3/7 5.5/5 5.7 5.5/6 6.3/10 5.7/11 5.5/15 5.6/30

4.3/30 4.8/24 4.4/22 4.6/11 5.4/10 4.4/6 4.0 4.3/5 5.1/9 4.2/10 3.6/15 3.1/30

5.6/30 6.3/24 5.6/22 5.5/12 6.4/10 5.5/7 5.1 5.3/5 6.2/9 5.5/10 4.6/17 4.6/30

5.9/30 6.6/23 6.2/21 5.9/10 6.8/9 6.0/5 5.7 5.8/6 6.8/9 6.6/10 5.9/18 4.3/30

8.2/30 8.7/22 8.1/21 7.9/10 8.7/8 7.9/6 7.5 7.8/6 8.6/9 7.8/10 8.3/12 8.2/19 7.8/30

8.6/30 9.0/22 8.6/21 8.4/10 8.9/9 8.0/6 7.7 8.0/6 8.2/8 7.6/9 8.4/20 9.1/25 9.1/30

6.3/30 7.0/24 6.7/19 8.2/7 8.5/6 7.7/3 7.6 7.7/4 7.4/10 8.4/14 7.6/15 7.4/17 7.7/20 7.6/26 7.9/30

6.3/25 5.3/22 6.3/30 4.8/10 5.2/7 6.1/5 7.0/4 6.4/2 6.0 5.5/5 6.0/11 6.7/13 5.9/14 5.7/17 4.2/21 3.9/27 3.8/30

8.4/30 8.5/28 7.7/26 6.8/18 6.6/8 6.8/6 7.8/5 7.0/2 6.6 6.3/5 6.7/9 7.5/12 6.5/14 6.2/16 3.7/25 3.7/30

8.3/30 8.5/19 8.7/11 9.7/9 8.5/5 8.5 8.6/7 9.7/10 8.4/12 8.5/22 9.3/25 8.9/30

Sta	+	H.I.	-	Elev.	Rem's
99+0		1114.02			
T.P.	3.825	1108.85	8.995	1105.025	
B.M.	2.86	1108.85	2.86	1105.99	Spike in N. Side 24" Elm 18' Rt. Sta 99+05
100+0					
101+0					
T.P	4.75	1108.04	5.56	1103.29	
102+0					
103+0					
103+38	℄ Drive South				
104+0					
T.P	2.93	1103.60	7.37	1100.67	
105+0					
B.M.			3.09	1100.51	Spike in S.W. Root 10" Poplar 50' Lt. Sta 105+15
106+0					

South ℄ North

9.3/30 9.1/17 9.3/7 10.4/5 9.6/2 9.1 9.2/4 9.5/9 10.4/12 9.9/13 9.7/15 9.1/18 9.2/30

5.3/23 4.8/19 5.0/16 5.4/8 5.1/5 6.0/4 5.6/2 5.4 5.1/4 5.4/9 6.0/11 5.4/13 5.0/17 4.5/20 4.6/30
5.4/30

Sta 100+0

6.4/30 6.3/23 5.8/20 6.0/16 6.3/8 6.1/6 7.0/5 6.0/2 5.7 5.5/4 5.8/9 6.8/12 6.0/13 6.3/20 6.1/30

Sta 101+0

4.7/30 4.7/20 4.6/15 5.5/11 5.5/7 6.3/6 5.2/3 5.1 5.0/8 5.4/11 6.3/14 5.5/16 5.6/23 6.0/30

4.1/30 4.2/20 4.7/10 5.6/8 5.2/7 6.3/6 5.1/3 5.0 4.7/4 4.9/8 6.3/11 5.3/13 5.2/20 5.6/30

(4.7/H) 5.1/30 5.1/9 6.2/5 5.7

6.8/30 6.2/19 6.7/10 7.3/8 8.0/6 7.0/3 6.8 6.6/5 6.9/7 8.2/11 7.5/12 7.5/14 6.7/18 7.0/30

2.8/30 2.9/25 3.1/19 3.9/10 5.2/8 4.2/5 3.9 4.3/6 5.2/8 4.7/10 4.8/14 5.1/30

6.1/30 6.0/19 5.9/11 6.3/9 5.8/8 5.5 5.5/5 6.0/7 6.6/9 6.3/11 5.6/18 5.9/30

Sta	+	H.I.	−	Elev.	Rem's	South ℄ North
		1103.60				
106+60					℄ Culvert	9.2/150 8.0/100 7.6/40 7.6/F.L. → 3.6/9.1 3.6/7.6 5.0/7.6 **4.9** 4.7/7.4 3.6/7.4 3.6/8.9 ← 7.9/F.L. 6.9/25 7.0/75 6.9/100; 9.7/160 9.5/175
107+0						5.7/30 5.8/21 6.4/11 6.8/8 6.2/5 **6.2** 6.2/8 6.7/10 6.0/11 5.8/17 5.0/20 4.8/30
108+0						(2.5/H) 3.8/30 5.1/19 5.2/11 6.1/9 5.7/6 **5.4** 5.8/6 6.5/8 5.5/10 4.6/17 4.1/30
+35					℄ Drive South	5.1/30 5.4/17 **5.2**
T.P.	5.58	1103.79	5.39	1098.21		
109+0						5.7/30 5.3/24 6.1/18 5.9/14 6.3/13 5.3/8 **5.3** 5.9/5 6.6/7 5.9/8 6.0/17 6.0/30
110+0						5.2/30 5.6/20 5.3/18 6.0/13 6.6/11 5.8/8 **5.4** 5.8/4 6.2/6 5.8/7 5.8/10 5.3/12 4.7/17 4.5/30
T.P.	3.84	1100.75	6.88	1096.91		
110+45					℄ Culvert	3.5/30 3.3/19 3.1/16 3.5/14 4.2/13 4.2/F.L. → 3.1/10 **3.1** 3.2/6 ← 4.0/F.L. 3.8/8 3.1/9 3.2/15 2.5/30
					Note: an outlet channel could be opened on South side if a new culvert is built	
+67					℄ Drive North	**3.4** 3.3/12 3.0/30 (0.1/H)
111+0						4.9/30 4.1/16 4.1/12 5.0/10 4.5/9 3.9/7 **3.7** 3.9/4 4.2/6 3.3/10 3.5/30
112+0						3.7/20 3.9/15 4.7/13 5.1/11 6.1/10 5.6/8 5.2/5 **4.8** 5.1/8 5.7/10 5.0/12 4.2/18 3.7/30; 4.6/30

Sta	+	H.I.	-	Elev	Rem's
113+0		1100.75			
B.M.	5.155	1100.79	5.115	1095.635	Spike in N.W. Root 16" Maple 31' Rt. Sta 113+62
113+71	±	Culvert			
114+0					
T.P.	5.29	1100.84	5.24	1095.55	
115+0	Swamp on South Side of Rd				
116+0					
117+0					
118+0					
+40					
T.P.	3.25	1101.47	2.62	1098.22	
119+0					
120+0					

South ℄ North

6.1 30	5.8 16	6.4 14	6.5 12	7.4 10	6.6 8	5.6 4	5.5	5.5 5	5.8 8	6.7 10	6.2 12	5.0 19	4.7 30
7.7 70	6.7 30	6.5 19	7.4 10	6.8 F.L.	6.2 8.5	5.5	5.9 7	6.2 7.5	6.8 F.L.	7.0 11	6.3 12	5.6 19	4.9 30
6.3 30	6.1 21	5.0 17	6.2 15	6.4 14	7.0 11	6.1 7	5.8	6.0 6	6.9 9	6.3 11	5.5 18	4.8 30	
7.4 30	7.3 25	6.4 23	6.7 13	7.3 12	6.0 7	5.7	5.8 6	6.6 9	6.0 10	5.4 30			
5.8 30	5.4 23	5.2 17	6.0 12	6.4 11	5.6 7	5.2	5.5 4	6.1 6	5.3 7	4.9 10	3.9 30		
6.0 30	5.5 22	5.2 13	5.5 11	5.0 8	4.3	4.7 4	5.3 6	4.4 7	3.1 30				
2.8 30	2.7 21	2.8 17	3.2 12	4.2 10	3.5 8	3.2	3.5 3	4.1 6	3.1 7	2.4 13	1.8 30		
3.7 30	2.9 22	2.7 12	3.6 10	2.8 8	2.7	2.8 3	3.2 5	2.1 7	1.6 15	1.0 30			
4.9 30	4.4 21	4.5 11	5.3 10	4.5 7	4.2	4.6 3	5.1 5	4.3 7	3.5 16	3.0 30			
5.8 30	5.6 25	5.2 20	5.5 12	6.3 10	5.7 7	5.3	5.6 3	6.3 6	5.4 7	4.6 30			

Sta	+	H.I.	-	Elev	Rem's
121+0		1101.47			
+68	℄ Culvert				
	* Last Reading taken in Creek running parallel to ℄.				
122+0					
B.M.			6.65	1094.82	Spike in W. Root 18" Maple 50' Rt. Sta 121+40.
T.P.	7.08	1102.71	5.84	1095.63	
123+0					
124+0					
+87	℄ Drive North				
125+0					
T.P.	2.30	1097.11	7.90	1094.81	
126+0					
127+0					
+80					

South ℄ North

6.5/30 5.9/20 6.5/10 6.8/9 6.5/7 6.1 6.3/5 6.9/7 6.4/9 5.7/20 6.0/30

10.6/55* 9.5/55 8.0/30 7.9/19 8.1/FL+9 7.5/7 6.6/7 6.1 6.4/4 7.3/7 7.5/8+FL 7.8/17 7.5/30 7.4/30

7.0/30 6.5/21 6.8/11 7.0/9 6.3/7 5.9 6.2/4 7.1/7 6.9/9 6.6/30

5.3/30 4.8/20 4.9/15 5.5/12 6.4/10 5.4/7 5.1 5.4/3 6.2/6 5.2/8 4.9/17 5.2/23 5.4/30

6.1/30 5.2/19 5.6/12 6.1/11 5.3/8 5.1 5.3/3 6.1/6 5.3/7 4.6/13 4.9/30

7.2 7.8/5 6.8/18 6.4/30 3.7/H

7.9/30 7.1/20 7.3/13 8.3/11 7.8/8 7.7 8.3/5 8.9/9 6.4/13 6.3/30

4.5/30 4.6/24 4.5/17 4.7/11 5.9/10 5.5/7 5.1 5.3/4 5.9/6 4.2/10 3.9/30

11.1/40 10.3/30 9.7/21 9.1/13 8.8/9 8.9/8 8.3/6 8.0 8.6/5 9.0/9 6.9/30

11.4/40 11.4/19 10.7/5 8.9/2 9.0 9.0/7 10.7/13 11.6/30

Sta	+	H.I. 1097.11	−	Elev	Rem's
128+0		2/50 CULVERT			
		* 70' N. of ℄ the Pres. outlet commences to run East (parallel with ℄ Rd.)			
+10					
T.P.	6.13	1095.32	7.92	1089.19	
129+0					
		Because of Thick			
130+0		Brush Readings			
		Were taken on South			
131+0		Side first			
131+75					
T.P.	3.12	1089.48	8.96	1086.36	
130+0					
131+0					
T.P.	4.23	1088.88	4.83	1084.65	
131+75					
132+0					

South ℄ North

12.0/60 12.3/45 12.1/30 12.7 F.L. + 3.5 7.9/2.5 7.9/2.5 8.5/2.5 8.5 8.5/9.2 7.9/7.2 7.9/10.2 ← 12.6 F.L. 12.7/30 * 12.8/70 10.6/100

10.7/40 11.0/30 11.1/24 10.2/5 9.0/3 9.2 9.2/7 11.9/15 11.7/21 12.0/30

5.4/26 5.2/24 6.0/20 8.9/14 9.3/9 10.2/7 9.2/5 8.8 9.0/8 9.8/10 9.4/13 9.1/16 9.0/24 8.8/30

4.7/27 5.0/30 4.9/40

7.0/40 6.9/31 6.6/30 6.3/26 6.9/23 6.8/17

7.3/40 7.2/34 7.3/30 7.7/26 8.5/22 8.9/18

7.6/40 7.6/35 7.9/32 8.7/30 9.3/25 10.0/21 11.1/16 11.6/10

7.9/14 3.3/12 3.8/10 2.9/8 2.7 3.0/3 4.4/8 3.6/9 3.4/14 4.4/19 5.1/22 4.7/30

3.4/18 4.9/14 5.4/13 5.2/11 5.2/2 5.1 6.0/1 5.1/3 5.6/7 6.1/12 6.6/14 7.1/15 6.8/19 5.9/21

5.4/25 4.6/28 4.2/30

5.3/10 5.8/9 5.3/7 5.3 5.3/4 5.5/5 4.9/6 5.5/15 5.9/20 6.4/24 7.0/27

6.9/30 6.7/32 5.5/38

3.4/40 4.1/34 5.2/30 5.3/24 5.1/12 6.1/10 5.5/9 5.3 5.3/5 5.6/6 5.0/8 6.4/18 6.5/27 7.1/30 7.0/34 5.6/38

Sta	+	H.I.	−	Elev.	Rem's
		1088.88			
T.P.	4.68	1089.31	4.25	1084.63	
132+61.4		℄ Culvert			
133+0					
B.M.			4.84	1084.47	Spike in N. Root 20" Maple 30' Rt. Sta 132+88
+10.94		℄ County Line Road			
+10.95		Culvert on County Line Rd. 54' South of Int.			

℄ Culvert is not ℄ of Rd.
(℄ Rd. 3' West of ℄ Culvert)
The Outlet Channel at a point 300' South of Rd. changes its direction from East to South. Then after 100' (South) it goes back to its orig. direction which is East

South ℄ North

83/30 8.0 T.B.→ 8.6/17 8.8 F.L.→ 4.0/2.3 4.0/1.3 4.7/1.31 4.6 4.7/10.2 4.0/10.2 4.0/11.2 8.8 F.L. 8.0/17 6.6/2.3 5.2/28 4.9/30

8.1/T.B. 8.6/40 → 6.9/T.B.

6.3/40 5.9/30 5.2/28 5.1/20 5.3 5.0/20 5.2/30 4.7/40

3.7/100 4.6/54 5.0/30 5.0 4.8/30 4.4/50 1.2/100 0.1/125

℄ Culvert on County Line Rd.

East

9.5/135 9.5/100 9.0/60 10.8/300 9.3 F.L.→ 11.7/375' 2.6/7 2.6/6 4.3/6 4.4 4.5/6 2.6/6 2.6/7 9.7 F.L.

West

Sta	+	H.I.	−	Elev	Rem's
B.M.	2.085	1137.56		1135.475	
0+40					
1+0					
2+0					
T.P.	5.78	1136.92	6.42	1131.14	
3+0					
4+0					
T.P.	3.03	1139.28	0.67	1136.25	
5+0					
+24					
6+0					
7+0					
T.P.	0.83	1129.04	11.07	1128.21	
8+0					
T.P.	1.57	1125.27	5.34	1123.70	

BURG TP. Sep. 12, 1930 Fair

S. Gold Jr.
S. Merritt
H. Barton

South	℄ Elevation		North
F. 4.0 / 22.0'	1135.72		F. 3.0 / 20.5'
F. 3.5 / 21.5'	1134.70		F. 2.5 / 19.9'
F. 2.5 / 19.7'	1133.14		F. 2.0 / 19.5'
F. 2.5 / 19.1'	1132.40		F. 1.5 / 19.3'
F. 2.0 / 20.0'	1131.80		F. 1.0 / 20.7'
C. 4.0 / 28.5'	1131.20		C. 7.0 / 32.0'
C. 5.0 / 29.5'	1131.06	C. 6.5 / 31.5'	
C. 4.5 / 28.7	1130.11		C. 4.0 / 27.9'
C. 4.0 / 26.3	1127.46		C. 1.5 / 24.1'
F. 0.5 / 21.0'	1124.20		F. 0.5 / 20.7

Sta	+	H.I.	-	Elev.	Rem's
		1125.27			
9+00					
10+00					
11+00				1118.68 Used	
B.M.	3.31	1121.99	6.63	1118.64	
12+00	Note: Open Ditch on South Side				
13+00					
T.P.	5.26	1122.87	4.38	1117.61	
14+00					
15+00					
T.P.	6.57	1123.25	6.19	1116.68	
16+00					
17+00					

South	℄ Elevation	North
C. 0.5 22.1	1121.00	Gr. 21.5'
F. 0.5 23.7	1118.91	C. 0.5 27.3'
F. 0.5' 25.1'	1118.73	C. 0.5 27.5'
F. 1.5 23.5'	1118.71	F. 0.5 27.5'
F. 1.5 25.0'	1118.69	F. 1.0 24.7'
F. 2.0 22.8'	1118.67	F. 1.5 27.0'
F. 2.0 27.0'	1118.69	F. 2.0 26.9'
F. 2.5 23.3'	1118.79	F. 2.0 23.7'
C. 2.5 24.1'	1118.89	C. 1.0 23.5

Sta	+	H.I.	-	Elev.	Remarks
		1123.25			
18+0					
B.M.	5.93	1124.32	4.89	1118.39 1118.36	
19+0					
20+0					
20+27					
T.P.	7.20	1123.71	1121.51		
21+00					
T.P.	5.10	1121.29	7.25	1116.19	
22+0					
23+0					
T.P.	5.87	1121.13	6.03	1115.26	
24+0					
25+0					

South	℄ Elevation	North
C.1.0 22.3'	1118.99	C.1.0 23.3'
F.0.5 20.7'	1119.09	F.0.5 20.9'
C.2.5 25.3	1119.06	C.1.0 23.5'
C.2.5 25.3'	1119.01	C.1.0 23.7
C.1.5 23.7	1118.62	C.0.5 22.7'
F.0.5 21.5	1117.86	F.0.5 21.1'
F.2.0 19.1'	1117.06	F.2.0 18.7
F.0.5 20.5	1116.26	F.1.0 20.3'
C.1.0 22.9	1115.46	Gr. 21.9'

Sta	+	H.I.	−	Elev.	Rem's
		1121.13			
26+0					
T.P.	5.03	1121.19	4.97	1116.16	
27+0					
B.M			4.01	1117.18	
28+0					
T.P.	7.53	1114.79	9.43	1111.76	
29+0					
30+0					
T.P.	3.03	1110.96	6.36	1107.93	
31+0					
T.P.	7.80	1107.58	6.18	1104.78	
32+0					
33+0					
34+0					

South	℄ Elevation	North
C. 3.5 / 26.9'	1114.66	C. 1.5 / 24.0'
C. 1.5 / 23.7	1113.86	C. 1.0 / 23.3'
F. 1.0 / 19.9'	1111.76	F. 1.0 / 20.0'
F. 1.5 / 19.0	1111.06	F. 1.0 / 18.3'
Gr. / 21.5	1108.93	F. 1.0 / 20.5
C. 1.5 / 24.7'	1106.01	C. 0.5 / 22.7
C. 1.0 / 23.0	1103.28	C. 1.5 / 24.1'
C. 0.5 / 22.3'	1102.46	C. 1.5 / 23.0
Gr. / 21.5	1101.96	Gr. / 21.7'

Sta	+	H.I.	-	Elev.	Remks
T.P.	4.08	1106.04		1101.96	
35+0					
36+0					
T.P.	4.54	1104.50	6.08	1099.96	
37+0					
B.M.			4.11	1100.39 Adj. 1100.39	
38+0					
39+0					
T.P.	4.71	1103.67	5.04	1099.46	
40+0					
41+0					
42+0					
B.M.			4.32	1099.36 1099.35	
43+0					
T.P.	3.50	1101.96	5.71	1098.46	

South	℄ Elevation	North
F. 0.5 / 71.3'	1101.46	F. 0.5 / 71.0
F. 1.0 / 70.5'	1100.96	F. 1.0 / 70.3'
F. 1.0 / 70.1'	1100.46	F. 1.0 / 70.5
F. 1.0 / 70.3'	1099.96	F. 0.5 / 70.9
F. 0.5 / 71.3'	1099.46	Gr. / 71.3
Gr. / 71.7'	1098.96	F. 0.5 / 71.8
C. 1.0 / 72.1'	1098.46	C. 1.0 / 72.7'
C. 0.5 / 72.5'	1097.96	C. 1.5 / 73.7'
C. 0.5 / 72.5'	1097.46	C. 1.0 / 73.1'

Sta	+	H.I.	-	Elev.	Rem's
		1101.96			
44+00					
45+00					
T.P.	3.61	1099.87	5.70	1096.26	
46+00					
47+00					
48+00		℄ Culvert			
	3.77	1094.13		1090.36	
48+57.5	PC.				
NOTE: Because of thick brush slope stakes set on So. Side only					
49+00					
T.P.	8.35	1097.55	4.93	1089.20	
49+50					
B.M.			8.55	1089.01 Rec. 1089.00	
50+00					

South		℄ Elevation		North
C.0.5 / 22.5		1096.66		C.0.5 / 22.7'
C.1.5 / 24.0		1095.26		C.1.0 / 23.5'
C.1.0 / 23.5'		1093.56		C.1.5 / 28.7'
F.1.5 / 19.7		1091.86		F.1.5 / 19.7'
		1090.69		
1090.74	F.1.0 / 21.0'	1090.50		1090.36
1091.20	F.1.0 / 22.3'	1090.58		1090.44
1091.19	C.1.5 / 22.9'	1090.79	F.4.0 / 26.0'	1090.65
C.1.0 / 23.3'		1091.26		

Sta	+	H.I.	-	Elev	Rem's
		1097.55			
54+0					
T.P.	9.76	1104.26	3.05	1094.50	
55+0					
55+50					
53+0					
54+0					
T.P.	8.18	1103.73	8.71	1095.55	
55+0					
55+40					
56+0					
57+0					

South ℄ Elevation North

C.1.0 / 22.9'	1093.50	C.1.0 / 23.3'
C.2.5 / 24.1'	1096.00	C.3.0 / 26.0
C.2.5 / 25.3'	1096.96	C.3.0 / 26.1'
C.0.5 / 21.7'	1097.35	Gr. / 21.7
F.V.0 / 19.1'	1097.55	F.V.0 / 18.7
C.0.5 / 22.3'	1097.75	C.0.5 / 22.5
	1097.83	
Gr. / 21.7'	1097.90	Gr. / 21.7'
C.1.5 / 24.3'	1095.75	C.0.5 / 22.9'

Sta	+	H.I	-	Elev.	Rem's
	2.79	1100.04		1097.25	
58+0					
59+0					
T.P.	2.92	1090.87	12.09	1087.95	
60+0					
B.M.			9.73	1081.14	
61+0	Stake Set on N Side only				
T.P.	4.29	1093.05	2.11	1088.76	
62+0	* Clean Present Ditch So. Side				
T.P.	10.65	1102.07	1.63	1091.42	
63+0	Grade to Present Ditch on So Side				
+84	Berm to be Widened on So Side				
64+0					
T.P.	6.96	1104.93	4.10	1097.97	
65+0					
T.P.	8.13	1111.00	1.06	1103.87	
66+0					
B.M.			2.78	1109.24 Rec. 1109.22	

South	℄ Elevation	North
C. 3.0 / 25.1	1092.15	C. 2.0' / 24.5'
F. 1.0 / 20.3'	1088.95	F. 1.5 / 19.9
F. 1.0 / 20.7'	1086.06	F. 0.5 / 21.5'
	1085.76	F. 4.5 / 22.5'
F. 3.5 / 24.7	1089.06	C. 2.5 / 25.7'
F. 2.5 / 22.0'	1094.95	C. 3.0 / 26.9'
F. 1.5 / 19.0'	1099.47	C. 3.0 / 26.0'
F. 1.0 / 19.0'	1100.26	C. 1.9 / 23.0'
C. 2.0 / 25.0'	1104.20	C. 2.5 / 25.5'
C. 1.0 / 23.3'	1106.89	C. 0.5 / 22.5'

Sta	+	H.I	-	Elev	Rem's
B.M.	4.73	1113.47		1109.24	
67+0					
68+0					
69+0					
T.P	6.78	1117.18	7.55	1110.95	
70+0					
71+0					
72+0					
+78					
73+0					
74+0					
75+0					

South	℄ Elevation	North
Gr. 21.9	1108.45	F. 0.5 / 20.7
C. 0.5 / 22.3	1109.45	F. 0.5 / 20.9
C. 0.5 / 22.3	1110.45	F. 0.5 / 21.1
Gr. 21.9	1111.83	F. 0.5 / 21.0
C. 1.0 / 22.9	1113.95	Gr. 21.3
C. 1.0 / 23.0	1115.93	Gr. 21.5
	1115.86	
C. 0.5 / 22.7	1114.75	F. 1.0 / 20.5
F. 0.5 / 20.7	1113.05	F. 1.5 / 19.9
Gr. 21.3	1111.56	F. 1.0 / 20.5

Oct. 16, 1930 Windy (Temp 26°)

Sta	+	H.I.	−	Elev.	Remarks
		1117.18			
76+0					
B.M.			5.06	1112.11 rec. 1112.12	
77+0					
T.P.	4.59	1113.91		1109.32	
78+0					
79+0					
80+0					
T.P.	4.72	1112.77	5.86	1108.05	
81+0					
B.M.			3.16	1109.60 rec. 1109.61	
82+0					
83+0					
T.P.	3.85	1112.18	4.44	1108.33	
84+0					

S. Gold Jr.
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N. Barton

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South	℄ Elevation	North
Gr. 21.0	1110.18	F.0.5 21.1
F.0.5 21.0	1109.82	F.0.5 20.9
F.0.5 21.0	1109.53	F.0.5 21.31
F.0.5 20.7	1109.29	F.0.5 20.7'
F.0.5 20.9'	1109.05	F.1.0 20.1'
F.1.0 21.0'	1108.81	F.1.0 21.0
Gr. 21.5'	1108.57	F.0.5 21.1'
F.0.5 21.5	1108.33	Gr. 20.9'
Gr 21.9'	1108.09	F.0.5' 21.1'

Sta	+	H.I.	-	Elev.	Rem's
		1117.18			
85+0					
86+0					
T.P.	4.26	1117.71	3.73	1108.45	
87+0					
88+0					
89+0					
B.M.	4.815	1117.75	4.80	1107.935 1107.91	
90+0					
91+0					
92+0					
93+0					
T.P.	3.38	1110.43	5.70	1107.05	

South	℄ Elevation	North
F.0.5 21.0'	1107.94	F.1.0 20.0'
Gr. 21.5'	1107.95	C.0.5 22.7'
C.1.5 24.5	1108.05	C.1.0 22.9'
F.0.5 21.1'	1108.15	F.1.0 20.5'
F.1.5 19.7	1108.25	F.1.5 19.5'
F.1.0 20.5'	1108.35	F.1.0 20.5'
Gr. 21.7	1108.45	C.1.0 23.7'
F.1.5 20.3'	1108.40	Gr 21.5
F.2.0 19.5	1108.05	F.1.0 20.0'

Sta	+	H.I.	−	Elev.	Rem's
		1110.43			
94+0					
95+0					
96+0	6.04	1114.59		1106.55	
+70					
97+0					
T. P.	3.81	1110.35	6.05	1106.54	
98+0					
B.M. & T.P.	2.50	1108.49	4.36	1105.99	
99+0					
100+0					
101+0					
T.P.	5.67	1108.22	5.94	1102.55	
102+0					

South ± Elevation North

F. 1.5 / 19.7' — 1107.55 — F. 1.5 / 19.7'

F. 1.5 / 19.7 — 1107.05 — F. 1.5 / 20.1

C. 0.5 / 23.1 — 1106.55 — Gr. / 21.7

C. 2.0 / 25.9' — 1106.20 — C. 4.0 / 28' — C. 4.5 / 28.5'

C. 0.5 / 23.3' — 1106.05

Gr. / 22.1' — 1105.55 — Gr. / 22.1'

F. 0.5 / 21.7' — 1105.05 — Gr. / 21.9'

1104.55

F. 0.5 / 21.5' — Gr. / 21.5'

F. 1.5 / 20.7' — 1104.05 — F. 1.5 / 20.0

Gr. / 21.9' — 1103.55 — F. 1.0 / 20.5

Sta	+	H.I.	-	Elev.	Rem's
		1108.27			
103+0					
104+0					
B.M.	3.85	1104.36	7.70	1100.51 / 1100.51	
105+0					
T.P.					
106+0	Special Ditches on Both Sides				
B.M.	3.86	1104.77		1100.51	
107+0	Special Ditches on Both Sides				
108+0					
T.P.	5.00	1103.90	3.87	1098.90	
109+0					
110+0					
111+0					
T.P.	3.69	1101.29	6.30	1097.60	

South	℄ Elevation	North
C.1.5 / 23.7'	1104.96	F.0.5 / 21.5'
Gr. / 24.0	1101.80	F.0.5 / 24.1'
C.0.5 / 22.3'	1100.55	F.1.0 / 21.0'
F.1.5 / 28.7'	1099.30	F.1.5' / 24.3
F.1.0 / 22.9'	1098.71	Gr / 24.1
Gr / 21.5'	1098.90	C.0.5 / 22.7
F.0.5 / 26.5'	1098.70	F.0.5 / 21.1'
Gr. / 22.0'	1098.29	C.1.0 / 23.5'
F.1.0 / 20.5'	1097.60	Gr. / 21.9'

Sta	+	H.I	-	Elev.	Rem's
		1101.29			
112+00					
113+00					
B.M.	4.66	1100.30	5.64	1095.635 1095.64	
114+00					
115+00					
116+00					
117+00					
T.P.	4.28	1101.95	2.63	1097.67	
118+00					
118+50					
119+00					

South	℄ Elev.	North
Gr. 22.5	1096.76	Gr. 22.0'
F.1.0 20.5'	1095.93	Gr. 21.9
Gr. 22.5	1095.40	Gr. 22.0'
F.1.0 20.3'	1095.48	Gr. 21.5
F.0.5 21.1	1096.17	C.0.5 22.5'
F.1.5 19.2'	1097.17	C.0.5 22.1
Gr. 22.5'	1098.03	C.1.0 22.9
Gr. 22.0'	1098.12	C.1.5 24.0'
F.0.5 21.0'	1097.93	C.0.5 22.5

Sta	+	H.I.	−	Elev.	Rem's
		1101.95			
120+00					
121+00					
B.M	6.55	1101.37	7.11	1094.84	
121+50					
122+00					
123+00					
+50					
124+00					
125+00					
T.P.	7.98	1098.36	5.99	1092.38	
126+00					

South	± Elevation	North
F.0.5 / 11.3'	1096.87	F.0.5 / 21.5'
F.0.5 / 11.9'	1095.67	Gr / 22.1'
	1095.47	
F.1.0 / 10.3'	1096.07	F.0.5 / 11.0'
Gr / 7 7.3	1097.8 7	Gr / 11.9'
F.0.5 / 11.5'	1098.07	F.0.5 / 11.7
F.0.5 / 11.5	1097.8 7	C.0.5 / 22.7'
F.0.5 / 11.5'	1095.88	C.0.5 / 22.7
Gr / 7 7.3	1097.57	C.0.5 / 22.9

Sta	+	H.I.	-	Elev	Rem's
		1098.36			
127+0					
T.P.	5.11	1094.5✓		1089.41	
127+10					
129+0					
130+0					
T.P.	6.34	1091.01	9.85	1084.67	
131+0					
132+0					
T.P.	6.35	1088.9✓	8.44	1082.57	
133+0					
B.M.			4.4✓	1084.6	
B.M.			2.19	1086.78	X on NE Corner E. Hdwall Culvert County Line Rd

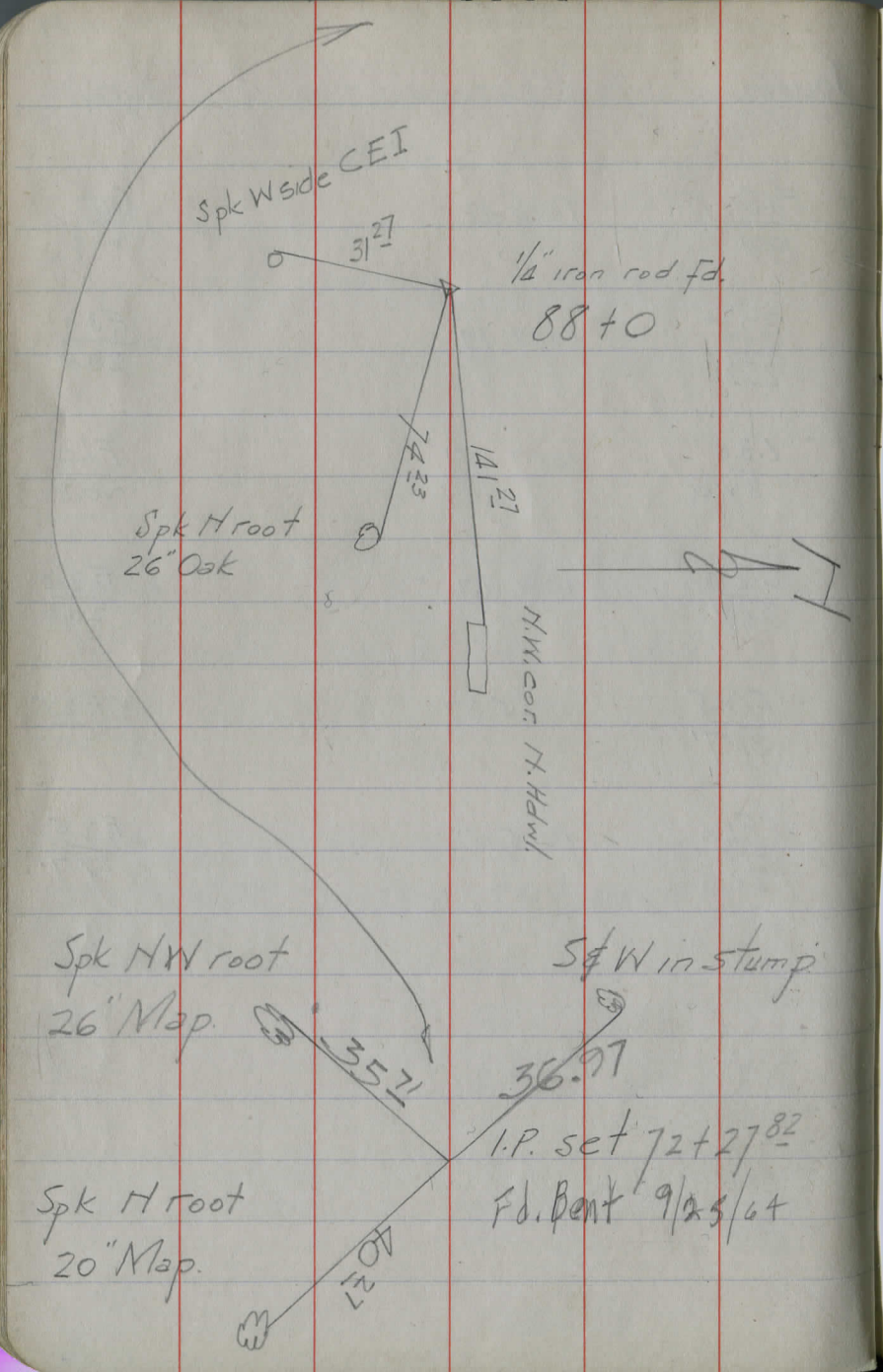
South	± Elevation	North
F. 1.5 / 19.3'	1089.41	GL ~1.9'
F. 2.5 / 25.3'	1088.19	F. 3.0 / 20.0'
C. 3.0 / 32.0	1087.47	F. 1.0 / 20.3'
C. 2.0 / 31.5'	1086.67	F. 2.0 / 20.0
C. 2.5 / 31.7'	1085.87	F 2.5 / 20.7
F. 1.0 / 28.0	1085.07	F 2.5 / 18.7'

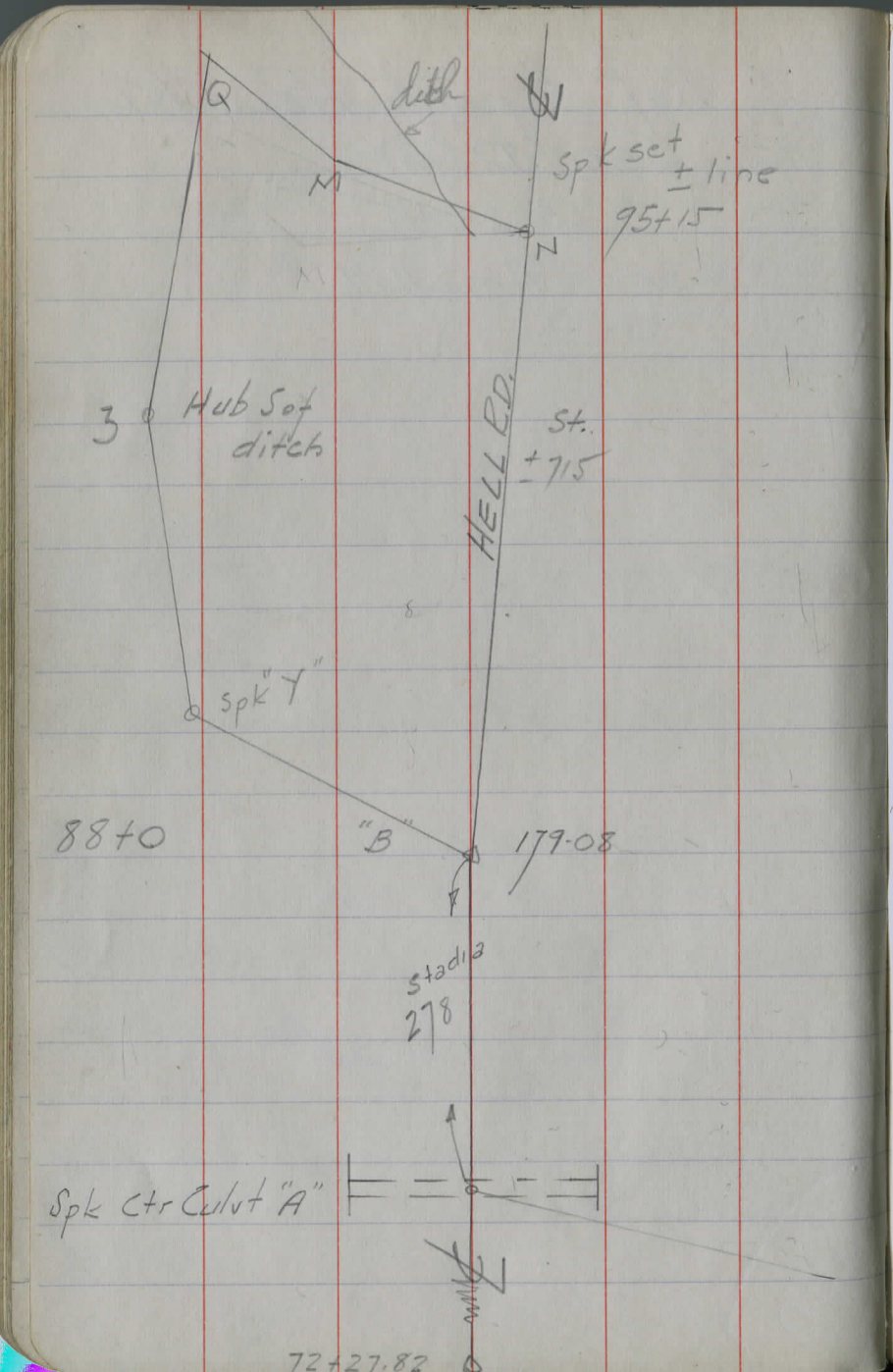
Ref. to points HELL RD

#116 SEC D (pt)

5-23-45

Form - Hall





5-23-45
Rom - Hall

8860
278
8582

DRAINAGE HELL RD
SEC "D" Sta 85 to Sta 100
& Vicinity

pgs 40 – 45

All dist. by stadia

BM #14	5.08	1111.07 ✓		1105.99
99+0				
98+0				
97+0				
96+0				
95+0				
94+0				
T.P.	5.69	1112.74 ✓	4.02	1107.05 ✓
93+0				
92+0				
91+0				
± 23	Drive pipe			
90+0				
+41		Culvt		
BM	5.10	1112.91 ✓	4.93	1107.81 ✓
89				
88				
+80	F.L. out 10" VSP			
±16	" in			
87				
86				

N ditch	E	S ditch	E
7.4	1103.7	7.5	1103.6
7.0	04.1	7.0	04.1
5.5	05.6	6.2	04.9
5.7	05.4	6.2	04.9
6.0	05.1	5.8	05.3
5.4	05.7	5.4	05.7
7.0	05.7	6.6	06.1
6.3	06.4	6.3	06.4
5.6	07.1	5.8	06.9
		6.95	out 05.8 12" Corr
6.2	06.5	6.7	06.0
7.51 out	05.23	6.98 in	05.76
N.W. Cor. N. Hdwl			
6.7	06.2	6.6	06.3
6.6	06.3	6.6	06.3
		6.63	06.3
		6.62	06.3
6.0	06.9	6.5	06.4
6.1	06.8	6.7	06.2

1112.91

+	Drive pipe (Corr)			
+55	" "			
+72	12" culvt (corr)			
+72	3" drain carry H_2O in 5/23/45			
BM			4.41	1108.50
85				

Set	Angtm.			
B	A	all ang to rt.		
BM	4.67	111°.48		1107.81
	141-31	180'	6.9	05.6
	123-52	252'	7.6	04.9
transit	129-33	251'	6.11	06.37
Level Hi =	1112.91		6.55	06.36
Set at A	Backsight E West	all ang to lt		
	107-02	115'	7.6	05.8
BM	4.92	113°.42		1108.50
	40-40	268'	7.5	05.9
Hi 1112.91	67-31	314	7.9	05.0

			5	113
	6.40 out ± 6.50 in	1106.5		
	6.90	06.0	7.40	05.5
			7.00	05.9

NW & N Hd WL

ditch N from culvt 89+41

" " " " N "

intersec. E & W ditch

Spk NW root (6' from trunk) 20" Elm

15' E of fence 15' S of ditch

H_2O standing

" "

FL 8" tile (thru break)

		1112.91		
Set at A	69-04	457	6.96	1105.95
" " X	5.18	1111.13		1105.95
	all ang rt			
X	159-40	169'	4.8	06.3
	150-52	514	4.3	06.8
	131-57	± 628	± 5.1	06.0
		+ 4.62		
Set Y	Ang from B	H.I. 1110.98		1106.36
	57-13 Rt	129'	6.3	04.7
	142-38 Lt	101'	5.8	05.2
	137-08 "	198'	5.9	05.1
	135-40	301	5.9	05.1
	slightly lighter ± 900' N (at Y)			
	134-22	314'	4.50	1106.48
	465	1111.13		1106.48
Set 3	all ang to Rt			
	181-52	131'	6.6	04.5
	182-30	288'	7.05	04.1
	185-42	420	8.2	02.9
	187-17	421	7.40	1103.73

— ground ele (tile ± 4' E) T.P. ≠ T.P.
Lights E & W

grd ± over tile
" " " "
" " " "

E & W ditch on Rudowski
ditch E
" "
" "

— guessed by sighting on fence post
T.P. ≠ Tran. Pt. 3 (Hub)

T.P. ≠ T.P. ℄

	6.99	1110.72		1103.73	Q
Set M	124-54 Lt	131	6.99		
	109-10 Lt	261	8.1	02.6	
			5.7	05.0	
		182			
T.P.			3.63	1107.10	(1107.05)
Set M		106-36	182		

Q
— ditch thru old R/W
inters. Rd ditch & ditch N & Ely
to M

to M from B

1124-54
15-45
109-10

10-17-53

Pioneer Road Drainage

NOTE: N. rd. ditch recently graded

BM	3.86	1111.67		1107.81
			6.37	05.30
90			5.7	06.0
+80			5.1	06.6
91			5.4	06.3
+41			5.3	06.4
92			5.8	05.9
93			6.5	05.2
94			6.8	04.9
95			7.3	04.4
96			7.2	04.5
T.P.	2.50	1109.02	5.15	1106.52
97			4.7	04.3
+85 =	± NWly line of ditch old RR R/W		5.6	03.4
98			5.7	03.3
99			6.1	02.9
100			6.8	02.2
101			7.4	01.6
102			7.8	01.2
103			8.1	00.9
104			9.7	1099.3

as in 1945 →

ditch still runs ± due N from culvt at 89+41

NW cor. N h'd w/ 89+41

← North F/L 7'E of culvt N. ditch 5.12

11-6-53 John Poms

PIONEER ROAD

+50				13.08 04.57 G 8.51 ✓	
92				13.08 04.68 G 8.40 ✓	
+50				13.08 04.80 G 8.28 ✓	
91				13.08 04.91 G 8.17 ✓	
+50				13.08 05.03 G 8.05 ✓	
90+0				13.08 05.14 G 7.94 ✓	
B.M	5.27	1113.08 ✓		1107.81	

N ditch stks S ditch 47

GRADES FOR N DITCH

N ditch	stks	S ditch
	8.51 5.91 r C 2.60 = 2'7"	
7.2	8.40 5.63 r C 2.77 = 2'9¼"	7.0
	8.28 5.48 r C 2.80 = 2'9½"	
6.8	8.17 5.54 r C 2.63 ✓ = 2'7½"	6.8
	8.05 5.40 r C 2.65 ✓ = 2'8"	
7.1	7.94 5.42 r C 2.52 ✓ = 2'6"	6.8

NW & NE dr'l

						N. Ditch	Sta.		S. Ditch	4/6
96					11.39 03.76 G 7.63 ✓	6.9	7.63 5.22 r C 2.41 = 2'5"		7.0 cattails	
+50					11.39 03.88 G 7.51 ✓		7.51 5.01 r C 2.50 = 2'6"			
95					11.39 03.99 G 7.40 ✓	7.0	7.40 4.86 r C 2.54 = 2'6½"		6.5	
T.P.	4.76	1111.39 ✓	6.45	1106.63 ✓						
+50					13.08 04.11 G 8.97 ✓		8.97 6.45 r C 2.52 = C2'6"			
94					13.08 04.22 G 8.86 ✓	8.4	8.86 6.30 r C 2.56 = C2'6¾"		7.8	
+50					13.08 04.34 G 8.74 ✓		8.74 6.14 r C 2.60 = C2'7"			
93		1113.08 ✓			13.08 04.45 G 8.63 ✓	7.9	8.63 6.04 r C 2.59 = 2'-7"		7.2	

		N. DITCH	STR	S. DITCH
			103+38 12" corr drive pipe to hse	
100				8.9
			+15	12" corr drive pipe to field
99				8.2
98	11.39 03.30 G 8.09 ✓	7.9	8.09 6.28 r c 1.81 = 1'10"	7.7
+50	11.39 03.42 G 7.97 ✓		7.97 5.87 r c 2.10 = 2'1"	
97	11.39 03.53 G 7.86 ✓	7.0	7.86 5.45 r c 2.41 = 2'5"	7.0
96+50	11.39 03.65 G 7.74 ✓		7.74 5.21 r c 2.53 = 2'6½"	
	1111.39 ✓			

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON O.
PHONE 250-X

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR FINDING BACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.

R.